PREPRINT

11 66246

11th ORDER RESONANCE TERMS IN THE GEOPOTENTIAL FROM THE ORBIT OF VANGUARD 3

C. A. WAGNER

(NASA-TM-X-66246) ELEVENTH ORDER
RESONANCE TERMS IN THE GEOPOTENTIAL FROM
THE ORBIT OF VANGUARD 3 (NASA) 32 p HC
\$3.75

CSCL 03B

Unclas
G3/13 04308

MAY 1973

GSFC

GODDARD SPACE FLIGHT CENTER

GREENBELT, MARYLAND

11th ORDER RESONANCE TERMS IN THE GEOPOTENTIAL FROM THE ORBIT OF VANGUARD 3

C. A. Wagner Geodynamics Branch Geodynamics Program Division

May 1973

Goddard Space Flight Center Greenbelt, Maryland

PRECEDING PAGE BLANK NOT FILMED

11th ORDER RESONANCE TERMS IN THE GEOPOTENTIAL FROM THE ORBIT OF VANGUARD 3

C. A. Wagner

ABSTRACT

The orbit of Vanguard 3 (1959-7A) is strongly resonant with 11th order and odd degree terms in the geopotential. It affords an excellent opportunity to determine a significant linear constraint between these terms. Tracking data on this satellite (in the form of mean Kepler elements) are analyzed over a 3 1/2 year period in the early 1960's, which ends with the orbit having just passed through perfect commensurability. The eccentricity and inclination show the deep resonance variations (up to 2×10^{-4} in e and .02° in i) with great clarity. Previous and current geopotential solutions fail to explain these perturbations. The analysis determined the following constraint for the deep resonant terms (in fully normalized harmonics):

$$10^{7}(C, S)_{\ell, 11} = (8.6 \pm 0.2, 7.8 \pm 0.2) = (C, S)_{11, 11} - 6.7(C, S)_{13, 11}$$

$$+ 16.2(C, S)_{15, 11} - 22.9(C, S)_{17, 11} + 19.5(C, S)_{19, 11} - 6.5(C, S)_{21, 11}$$

$$- 7.2(C, S)_{23, 11} + 11.3(C, S)_{25, 11} - 5.0(C, S)_{27, 11} - 3.6(C, S)_{29, 11} + \cdots$$

If these 11th order coefficients are of the order of $10^{-5}/\ell^2$, there will be a significant contribution to this constraint for terms at least as high as (25, 11).

PRECEDING PAGE BLANK NOT FILMED

CONTENTS

	Page
INTRODUCTION	1
ANALYSIS	6
RESULTS	10
DISCUSSION	11
CONCLUSIONS	14
ACKNOWLEDGMENT	15
REFERENCES	16
TABLES	
<u>Table</u>	Page
1 Mean Element Observations of Vanguard 3 (1959-7A), 1961-64	19
2 Results of ROAD-Vanguard 3 Orbit Determinations (Using	
3-1/2 Years of GSFC Mean Elements)	23

Preceding page blank

Figure		Page
1	Measurement Residuals in Inclination From a 5 Year	
	Nonresonant Vanguard 3 Trajectory	24
2	Inclination Residuals From Two 5 Year Simulated	•
	Vanguard 3 Trajectories	25
3	Measurement Residuals in Eccentricity From a 5 Year	
	Nonresonant Vanguard 3 Trajectory	26
4	Vanguard 3 Constraint From Various Fields	27

11th ORDER RESONANCE TERMS IN THE GEOPOTENTIAL FROM THE ORBIT OF VANGUARD 3

INTRODUCTION

The subject of orbital resonance and its application to the determination of the geopotential has had extensive discussion in the literature (i. e., Cook, 1961; Morando, 1962; Blitzer, 1962; Allan, 1965 & 1967; Kaula, 1966; Kozai, 1966; Garfinkel, 1966; Gedeon, 1969; Gaposhkin & Lambeck, 1970, and King Hele, 1972a, among many, many other authors and papers). In fact a whole symposium was held on the subject in January, 1968 at TRW Systems Group, Redondo Beach, California. At that time there was a hope that the longitude dependent geopotential (to a fairly high degree) could be determined completely from the strong long term deviations of commensurate orbits. Indeed, there were a number of proposals (i. e., Greene, 1967; Gedeon, Private Communication, 1968) then to launch one or a series of special satellites to sample a large number of resonant orbits for just this purpose. But it was soon recognized that the magnitude of such a program was prohibitive especially in view of the many deep and nearto-resonant orbits already available for analysis (Wagner & Douglas, 1969). Indeed by the early 1970's the gravity harmonics of order 12, 13 and 14 (and past degree 20) had been so determined from near resonant, close orbits [Gaposchkin and Lambeck, 1970; Lerch et. al., 1972a]. The deviations of the distant communications satellites in deep resonant (commensurate) orbits have served as excellent independent proof that the low order and degree terms of recent comprehensive solutions (from precise orbit tracking) have considerable accuracy [Wagner, 1972a].

The possibilities of exploiting existing resonant orbits seemed exhausted by 1971. However, as Gaposchkin and Lambeck [1970, p. 20] noted, there does not exist a general theory of orbital resonance, and this should have been a warning that these possibilities were far from closed. Indeed, examination of the orbital tracking data discarded by the Smithsonian Astrophysical Observatory during preparation of their Standard Earth 2 (SAO SE 2) [Gaposchkin, 1970; Gaposchkin and Lambeck, 1970] reveals (with a shock) that all were orbits suffering from fairly strong or deep resonance effects. These were the 9th order resonant orbit of Telstar 1, and the two 11th order deeply resonant orbits of Vanguard 2 Rocket and Vanguard 3. It is ironic that the actual solution of the long period resonance problems in these orbits was not (as elaborately discussed in Gaposchkin and Lambeck, 1970) through selective editing of analytic resonant terms. The solution was to eliminate the offensive data altogether!

The other line of evidence that the possibilities are not closed stems from the remarkable new investigations by King Hele's group (i. e., Gooding, 1971a; King-Hele, 1972b) of 15th order resonances on close satellite orbits dragged (by the atmosphere) slowly through commensurabilities. These new effects were originally observed as an incidental mysterious perturbation in the inclination evolution of the orbit of Ariel 3, studied to reveal the "super-rotation" of the upper atmosphere.

The observations were of a seeming step decline in the inclination. On closer examination the evolution was actually a continuous oscillation of increasing amplitude and period, finally "reflected" at a critical point, not at mid cycle, into an oscillation of decreasing amplitude and period. The critical

point (of reflection) was found to be at the time of exact commensurability for the orbit with 15th order terms in the geopotential [Gooding, 1971b]. R. R. Allan, 1971 gives the full explanation for this curious unexpected behaviour as an example of an orbit being dragged through a resonance. When the drag forces are constant and dominate the resonance forces along track during the passage through commensurability, there is an exact solution for the inclination change in terms of Fresnel integrals. This solution displays the reflection characteristics and the building and decaying oscillations observed in the Ariel data.

Using the observed inclination changes together with the observations of the satellite's longitude, Gooding (1971b) derived a linear constraint among all the 15th order and odd order terms in the geopotential from the orbit of Ariel 3. His simple theory was Allan's (1971) formulation of the appropriate inclination rates due to the resonant geopotential terms. (Kaula's [1966] formulation for the geopotential rates is completely equivalent and will be used in what follows.) Because the orbit was nearly circular only one linear constraint could be easily derived. But the way was now open for deriving many other such constraints from close orbits observed during resonance passage (King-Hele, 1972b).

In theory every satellite is a candidate for an infinite number of such passage events which could be used for geopotential determination. In practice though, the far satellites will decay too slowly to reach these points in a reasonable time, while the close ones will pass through them too fast to be of much use. However there is still a large number of medium altitude satellites, with perigees between about 500 and 600 km whose orbit decay is just right for observing at least one such strong event within 5 to 10 years from launch. And for the more eccentric orbits with these perigees, there is the possibility of observing two or more series of resonances in each passage.

The orbit of Vanguard 3 and Vanguard 2 rocket [n (the 2 body mean motion) ~11revolutions/day, e (orbit eccentricity) = .19, perigee height = 520 km] is of this multiple resonance type. These Vanguard orbits offer the only opportunity to see significant 11th order geopotential effects similar to the unique opportunities afforded the 15th order dragged resonance orbits. But this opportunity has not been properly exploited. Indeed the Smithsonian has abandoned them altogether. Thus it can be fairly said that 11th order terms, until now, remain among the most poorly determined in the geopotential (see Discussion). Unfortunately, Vanguard 3 has only been well observed through the first strong resonance (in 1963-64) which was with odd degree terms proportional to e² and thus relatively weak. In 1966-72 however, its orbit passed through 3 potentially stronger resonance series with even and odd degree terms (still 11th order) proportional to e and 1. And in 1973-74 it should be passing through another strong resonance (similar to the 1963-64 commensurability).

But all of this history is fine hindsight. Even the first resonance pass was unknown to me when I examined a set of 182 mean Kepler elements for Vanguard 3, calculated by T. Heuring (private communication, 1972) from the Smithsonian's precision reduced Baker-Nunn camera observations (Table 1). I knew Gaposchkin and Lambeck's (1970) difficulties with this orbit and that it was strongly affected by drag (especially during the solar cycle high of the very early 1960's). My main concern was whether the orbit program I was using [see: Wagner and Douglas, 1970] could handle the strong and variable drag on a 3 1/2 year trajectory. This program, ROAD (Rapid Orbit Analysis and Determination), integrates orbits seminumerically using model atmospheres due (originally) to Jacchia, 1965 and 1971. In the integrator only terms not containing the satellite's mean anomaly are retained. In this sense the program generates mean elements under a wide variety of forces.

But it also can employ empirically derived secular rates and accelerations of the elements (to the 5th power). These were found necessary to keep the alongtrack deviations of Vanguard 3 to less than 2° over the long arc when integrating with either model atmospheres. (At this level, the longitude of the computed satellite is sufficiently accurate to obtain realistic resonant geopotential terms.) After a considerable amount of orbital experimentation in ROAD, a 3 1/2 year nonresonant trajectory (with drag and radiation effects) was computed for Vanguard 3, with less than 2° along-track variation from the observed elements. This trajectory used the Smithsonian Standard Earth 2 zonal geopotential coefficients. My original hope was to "see" the resonance in the drag affected mean anomaly observations, but the errors in the model atmosphere were too great to allow this. However the comparison of the inclination of this computed trajectory (only slightly affected by drag) with the "observed" mean elements showed a clear but unexplained oscillation of increasing amplitude, breaking off near the middle of a cycle at the end of the data (Figure 1).

This oscillation-breakoff was, of course, reminiscent of the dragged-resonance phenomenon so well explained by Allan (1971) for near circular, uniformly dragged orbits. Could these residuals be due to the same phenomenon on an eccentric orbit subject to a more complex drag-resonance regime? The answer was supplied by simulating a Vanguard 3 resonant trajectory with all relevant terms for the geopotential harmonics (11, 11) and (12, 11) (from the Standard Earth 2) and comparing it with the non resonant trajectory computed previously. The form of the inclination residuals produced (Figure 2) emphatically showed that the resonant terms would account for the phenomenon. It remained to identify and solve for the harmonic constraint(s) that would reproduce the observed inclination variations.

ANALYSIS

Kaula [1966, p. 49] identifies geopotential resonance as occurring when the orbit longitude ψ is stationary with respect to a particular gravitational harmonic term (ℓ, m, p, q) : thus

$$\dot{\psi}_{\ell, m, p, q} = 0 = (\ell - 2p) \dot{\omega} + (\ell - 2p + 1) \dot{M} + m(\dot{\Omega} - \dot{\theta}),$$
 (1)

where ω , μ , and Ω are the orbit's argument of perigee, mean anomaly and right ascension of the ascending node and $\dot{\theta}$ is the rotation rate of the earth. For Vanguard 3, the mean motion (\dot{M}) is close to 11 revolutions/day, which, since $\dot{\omega}$ and $\dot{\Omega}$ are comparatively small, establishes m=11 as the lowest order resonant term (under the specification ℓ - 2p + q = 1). Rewriting (1) for these terms, leaves only the q index unspecified:

$$\dot{\psi}_{res} = 0 = (\dot{\omega} + \dot{\mathbf{M}}) - q\dot{\omega} + 11(\dot{\Omega} - \dot{\theta}),$$

from which;

$$q(res.) = [11(\dot{\Omega} - \dot{\theta}) + (\dot{\omega} + \dot{M})] / \dot{\omega} . \tag{2}$$

From Figure 1, commensurability occurs in the neighborhood of 38400 MJD at which time the observations show $\dot{M} \doteq 3992.4$ degrees/day, $\dot{\omega} \doteq 4.9$ degrees/day and $\dot{\Omega} \doteq 3.3$ degrees/day. The solution of (2) (using $\dot{\theta} = 360 \cdot 985$ degrees/day) is very close to q (res.) = -2. Since $\ell - 2p + q = 1$, then $\ell = 3 + 2p$ and ℓ is odd. Thus the resonant series for this commensurability passage is: $(\ell, m, p, q) = (\ell, 11, (\ell - 3)/2, -2), \ell = 11, 13, 15, \ldots$ The resonant longitude ψ for this series is simply

$$\psi_{\text{res}} = 3\omega + M + 11(\Omega - \theta) \tag{3}$$

The observed variation of $\psi_{\rm res.}$ (= $\psi_{11,-2}$) is shown at the bottom of Figure 1 and the stationary value is indeed near the break in the last cycle (~38360 MJD).

And since it does become stationary, I chose to base the constraint on the determination of the inclination rate (İ) which is always well behaved during the passage. This rate (due the geopotential) is given from the Lagrange planetary equations [Kaula, 1966, p. 29] as:

$$\dot{\mathbf{I}} = \frac{\cos \mathbf{I}}{\operatorname{na}^{2}(1 - e^{2})^{1/2} \sin \mathbf{I}} \frac{\partial \mathbf{T}}{\partial \omega} - \frac{1}{\operatorname{na}^{2}(1 - e^{2})^{1/2} \sin \mathbf{I}} \frac{\partial \mathbf{T}}{\partial \omega},$$

where;

$$T = \frac{\mu a_{e}^{\ell}}{a^{\ell+1}} \sum_{\substack{\text{relevant} \\ \ell, \, m, \, p, q}} F_{\ell \, mp}(I) \, G_{\ell \, p \, q}(e) \, S_{\ell \, mp \, q}(C, \, S, \, \omega, \, M, \, \Omega, \, \theta),$$

and;

$$\mathbf{S}_{\ell_{\mathrm{mpq}}} = \begin{bmatrix} \mathbf{C}_{\ell_{\mathrm{m}}} \\ -\mathbf{S}_{\ell_{\mathrm{m}}} \end{bmatrix}_{\ell_{-\mathrm{m}} \; \mathrm{ODD}}^{\ell_{-\mathrm{m}} \; \mathrm{EVEN}} \cos \psi_{\ell_{\mathrm{mpq}}} + \begin{bmatrix} \mathbf{S}_{\ell_{\mathrm{m}}} \\ \mathbf{C}_{\ell_{\mathrm{m}}} \end{bmatrix}_{\ell_{-\mathrm{m}} \; \mathrm{ODD}}^{\ell_{-\mathrm{m}} \; \mathrm{EVEN}} \sin \psi_{\ell_{\mathrm{mpq}}},$$

with the orbit longitude defined (again) as:

$$\psi_{\ell \, \text{mpq}} = (\ell - 2p) \, \omega + (\ell - 2p + q) \, M + m(\Omega - \theta).$$

In the above expressions, μ is the earth's Gaussian gravity constant, a_e is its mean equatorial radius and a is the orbit's semimajor axis. The f functions are sinusoidal and the G functions are generally monotonic of order $e^{|q|}$ [see Kaula, 1966, p. 37]. The C_{ℓ_m} and S_{ℓ_m} are the usual gravitational harmonic coefficients. For the resonant series defined above, ℓ - m is even, and ψ (= $\psi_{res.}$) is the same for each term in the series. The rate due to the combination of these terms is then found to be simply:

$$\dot{\mathbf{I}} = \left[\sum_{\substack{\text{resonant} \\ \ell}} \mathbf{C}_{\ell,11} \mathbf{f}_{\ell} \right] \sin \psi_{\text{res.}} + \left[\sum_{\substack{\text{resonant} \\ \ell}} - \mathbf{S}_{\ell,11} \mathbf{f}_{\ell} \right] \cos \psi_{\text{res.}}, \tag{4}$$

where

$$f_{\ell} = \frac{\mu a_{e}^{\ell} F_{\ell, 11, (\ell-3)/2} G_{\ell, (\ell-3)2, -2}}{n a^{\ell+3} \sin I (1 - e^{2})^{1/2}} [11 - 3 \cos I] .$$
 (5)

Clearly, only the sum of the sine and cosine terms (in brackets) in equation (4) are what can actually be determined from observations of the variations of the inclination with (the slowly changing) orbit longitude.

Calling these terms the lumped coefficients of the 11th order ${\bf C_{11}}$ and ${\bf S_{11}}$, the two constraints which can be found from the I data are:

$$(C_{11}, S_{11}) = (\sum C_{\ell, 11} f_{\ell}, \sum -S_{\ell, 11} f_{\ell}).$$
 (6)

Evaluating the f_{ℓ} from (5) for the average Vanguard 3 orbit in the resonance pass (a = 1.332 earth radii, e = 119, I = 33.3°; the μ /n is irrelevant since it does not depend on ℓ), and normalizing with respect to the (11, 11) term gives the explicit determinable constraint as:

$$(C, S)_{11} = (C, S)_{11, 11} - 6.7(C, S)_{13, 11} + 16.2(C, S)_{15, 11}$$

$$- 22.9(C, S)_{17, 11} + 19.5(C, S)_{19, 11} - 6.5(C, S)_{21, 11} - 7.2(C, S)_{23, 11}$$

$$+ 11.3(C, S)_{25, 11} - 5.0(C, S)_{27, 11} - 3.6(C, S)_{29, 11} + \cdots,$$

$$(7)$$

where the $(C, S)_{11}$ of (6) and the (C_{11}, S_{11}) of (5) differ only by an irrelevant constant factor.

At this point Gooding, (1971b) solved directly for the lumped coefficients from sets of differenced I values (with observed values of $\psi_{\rm res.}$) for Ariel 3, using a least squares fit to Equation (4). I chose a more hazardous, though potentially more satisfying method to find these coefficients. The method was to solve for a set of (15, 11) coefficients from the same program (ROAD) which revealed the resonance effects (Figure 1). The hazard taken was in the attempt to use all the data in this determination. As I mentioned earlier, the

drag model does have deficiencies which, even solving for empirical secular terms as high as the fifth power in the mean anomaly; still leaves the computed orbit longitude with peak errors of as much as 1 1/2 degrees. But this level appears adequate for a decent discrimination of these coefficients. The advantage of the method, of course, is more complete use of the tracking data. In particular, the eccentricity shows the same peculiar dragged-resonance variations as the inclination (Figure 3), This variation adds to the strength of the constraint determination set up for the inclination data, [Equation (7)]. But it cannot be used to determine an independent constraint for these terms. In fact the eccentricity and inclination variations from these resonant terms are in phase and differ only by a constant or bit-factor; namely [from, Kaula, 1966, p. 40]

endendi maili essos intenco entre $\frac{(1-e^2)^2 dt e^2}{\sin T} \frac{(1-e^2)^2 dt e^2}{(1-e^2)^2 \sin T} \frac{(1-e^2)^2 dt e^2}{(1-e^2)^2 dt}$. $\frac{(\Delta e/\Delta I)_{res}}{(1-e^2)^2 dt} = \frac{(1-e^2)^2 dt e^2}{(1-e^2)^2 dt} \frac{(1-e^2)^2 dt}{(1-e^2)^2 dt} \frac{(1-e^2)^2 d$

"This ratio is 0.663 for Vanguard 3. Comparison of the variations in Figures

(1) and (3) gives the same ratio from the actual data. A comparison of the variations in Figures

The solution (in ROAD) for (15, 11) used the Standard Earth 2 with all its and the standard Earth 2 with all

to influence the (15, 11) solution as little as possible. A similar downweighting for the ω and Ω data was found to be necessary because of unresolved systematic errors in these arguments. The cause is probably drag again, but not directly. The computed semimajor axis shows (even in the final solution) a quadratic deviation from the observations of up to 100 m, over the 3 1/2 year data span. This is enough to explain the "cubic" Ω and ω residuals by way of errors in the computed secular rates of these arguments due to oblateness. But even with these model deficiencies, the least squares fit of the (15, 11) coefficients to the element data produced a dramatic reduction in the residuals for the inclination and eccentricity. The overall results of the differential correction is shown in Table 2. Also shown in this table are comparison solutions with the unadjusted resonance terms of the Standard Earth 2 and the Goddard Space Flight Center's (Goddard Earth Model) Gem 4 Field [Lerch et. al., 1972b] as well as with the original non resonant field. The Gem 4 included data from the deeply resonant Vanguard 3 and Vanguard 2 rocket body orbits. The significance of these test results will be discussed shortly.

RESULTS

The normalized harmonics found from the straightforward ROAD differential correction process (described in more detail by Wagner, (1972b) for a multi-arc zonal solution) was:

$$10^{7}(C_{15,11}, S_{15,11}) = (0.32 \pm 0.01, 0.73 \pm 0.01),$$
 (8)

with a correlation coefficient of -0.51 between these terms. I was pleased to find that the correlations of (15, 11) with the empirical terms in the mean anomaly were all less than |0.1|. This poorly determined data was apparently not

influencing the solution because of its deliberate downweighting. But the real proof of these speculations, indeed of the (too simple?) constraint theory itself, must be to derive a result from that theory and then test it against the data.

Evaluation of (7) with these adjusted (15, 11) terms and the (11, 11) and (13, 11) terms in the Standard Earth 2 (included in the trajectory) yields the following values for the Vanguard 3 resonance constraint:

$$10^{7}(C, S)_{11} = (8.6 \pm 0.2, 7.8 \pm 0.2)$$
 (9)

Equations (7) and (9) provide the means to obtain a single additional pair of coefficients for a field. For example, the constraint using the Standard Earth 2 field requires (17, 11) to be:

$$10^{7}(C, S)_{17, 11} = (-.457, .149),$$

which appears quite reasonable according to the simple rule proposed by Kaula, (1966) $[(C,S)_{\ell,m} \approx 10^{-5}/\ell^2]$. However, as can be seen from (7) this result is undoubtedly an accident because the effects of higher degree terms are far from negligible. Nevertheless this coefficient set is consistent with the Vanguard constraint and should fully explain the eccentricity and inclination residuals. Indeed the trajectory calculated in ROAD with this (17, 11) set was the equivalent of that calculated with the (15, 11) adjusted values, as shown also in Table 2. While this result was expected, it was still enormously gratifying as an elaborate numerical confirmation of the simple constraint.

DISCUSSION

The results of the previous section can best be summarized in a C, S diagram for the 11th order constraint (Figure 4) which emphasizes the relative superiority of the SAO SE 2, over the later Gem 4 solution. Clearly neither

solution comes close to explaining the resonant eccentricity and inclination variations (see also Table 2). But why does the SAO SE 2 field, which does not include any resonant Vanguard data, provide a better fit than the Gem 4 which does? It is not so surprising when it is recalled that the 7 day arcs of the Gem 4 solution would see very little of the variation in these long term effects. Gaposchkin and Lambeck (1971, p. 21) felt that analytic term selection might solve this problem in their approach. (The idea is to use only those terms which have periods of the order of the arc length: inherently impossible with straight numerical integration as used for the orbits in the Gem's). It is interesting that an unpublished SAO 1969 satellite-only solution called B6.1, with 11th order resonance terms through 16, 11 and using Vanguard 3 data, does come closer to the mean element constraint than any other recent SAO or Goddard field. The Smithsonian analytic (really semi-analytic) solutions use 30 day arcs where possible. This is clearly an advantage where long period resonance is encountered. But apparantly it is not sufficient where some terms are considerably longer than a month, (as in this case). On the other hand, in spite of the fair success of the B6.1 solution, it is possible that SAO abandoned this data only because the solutions with it were so highly correlated that the results were unrealistic. But that result might have been anticipated and a priori constraints applied to limit the coefficient solutions. My own feeling is that since it is never a matter of just one term with a very long period, but a spectrum of terms which cannot all be absorbed properly, the resulting solution will tend to be both unrealistic and highly correlated if only the long period terms are ignored.

Another comparison solution, Gem 2, (Lerch et al., 1972a), is also shown in Figure 4. It differs from Gem 4 only in that it lacks electronic-satellite data. The impact on the Vanguard constraint is obviously not significant.

What is significant is the probable impact of the odd degree terms beyond the 15th. Using the Kaula rule to estimate the size of the neglected coefficients, and taking the root sum of squares of the estimated terms [in Equation (7)] gives the concentric circles (of uncertainty) in Figure 4. These circles can be regarded in two ways. On the one hand they say that the recent comprehensive geopotential solutions (without Vanguard 3 data) can not be expected to reproduce the Vanguard constraint because of likely contributions beyond those solved for in these models. On the other hand they show that solutions for coefficients beyond about the 25th degree will benefit strongly from this constraint.

Of course, even for the less complete solutions, the constraint could still be used (as in the previous section) to satisfy a set of "lumped" coefficients tailored for the Vanguard 3 orbit.

Beyond the 11th order commensurabilities associated with this resonance pass (in 1963-64) are series for m=22, (associated with q=-4), m=33 (q=-6), and so on. But the lowest degree's for these are higher (22 and 33 (etc.)) and the resonant variations are proportional to e^4 and e^6 (etc.). Thus it can be expected that their effects will be slight compared to the 11th order series. In fact I have made a solution for (22, 22) from this data and the result was an insignificant determination with no appreciable change in the residuals.

However, the effects of the even degree "side band" resonances of 11th order (terms with q = -1 and -3) cannot be so easily dismissed. Their frequencies are distinct enough throughout the pass to be able to discriminate two sets of even order terms. Unfortunately the data is heavily weighted on the "high" side of the commensurability. This catches the longer (and shortening) period,

but lesser effects of the (previously commensurate) q = -3 terms. From MJD 37315 to 38602 (the span of the best data), the period of these effects falls from 165 to 75 days. The period of the potentially stronger q = -1 terms (commensurable later, in 1966) lengthens from only 45 to 82 days during this time span. Preliminary determinations of these constraints are promising but so far inconclusive. At any rate, these determinations are essentially uncorrelated with and do not significantly disturb the q = -2 constraint.

It is anticipated that a fairly strong constraint for even degree (11th order) terms will be determinable by the new mean element method from the q=-3 commensurability which was well observed (by precise Baker Nunn tracking) in 1959-1960. Unfortunately, only field reduced optical and X-band North American Air Defense Command Tracking is available to observe the probably much stronger q=-1, 0, and +1 commensurabilities in the late 1960's and early 1970's. But their greater strength should provide other sets of independent constraints for the even and odd degree terms.

CONCLUSIONS

A strong constraint has been found for 11th order and odd degree terms in the geopotential which have previously been poorly observed. This has been accomplished from analysis of mean element "observations" of the deep resonant orbit of Vanguard 3 in 1961-1964. The constraint is not satisfied by recent comprehensive geopotential solutions, some of which have used (improperly) Vanguard 3 tracking data. However the constraint is undoubtedly more strongly affected by terms above the 15th degree than those below, the latter being the only ones so far determined in these solutions. Because of this, the determined

condition equations (probably) will only be useful in achieving accurate geopotential results when solutions for terms as high as the 25th degree are attempted.

Examination of independent 11th order commensurabilities for Vanguard 3 in 1959-60, 1966-71 and 1973-74 (using mean elements derived from tracking data) should provide additional strong constraints for 11th order harmonics.

ACKNOWLEDGMENT

Special thanks are due Ted Heuring for supplying the excellent mean elements which were the basis for this study, and Barbara Putney for keeping the ROAD program on the road to the solutions.

REFERENCES

- Allan, R. R., Resonant Effect on Inclination for Close Satellites, <u>Royal Aircraft</u>
 Establishment Technical Report 71245, Farnborough, Hants., England, 1971.
- Allan, R. R., Satellite Resonance with Longitude Dependent Gravity, Effects
 Involving the Eccentricity, Planetary and Space Sciences 15, 1829, 1967.
- Allan, R. R., On the Motion of Nearly Synchronous Satellites, Proceedings of the Royal Society of London A, 288, 60-68, 1965.
- Blitzer, L., E. M. Boughton, G. Kang and R. M. Page, Effect of Ellipticity of the Equator on 24-Hour Nearly Circular Satellite Orbits, J. of Geophys. Res. 67, 329, 1962.
- Brouwer, D., Solution of the Problem of Artificial Satellite Theory without Drag, Astron. J. 64, 378-397, 1959.
- Cook, A. H., Resonant Orbits of Artificial Satellites and Longitude Terms in the Earth's External Gravitational Potential, Geophysical Journal 4, 53-72, 1961.
- Gaposchkin, E. M., Improved Values for the Tesseral Harmonics of the Geopotential and Station Coordinates, In: <u>Dynamics of Satellites 1969</u>, 109-118, Springer-Verlag, New York, 1970.
- Gaposchkin, E. M. and K. Lambeck, 1969 Smithsonian Standard Earth 2,

 Smithsonian Astrophys. Obs. Special Report 315, Cambridge, Mass., 1970.
- Garfinkel, B., Formal Solution in the Problem of Small Divisors, Astron. J. 71, 657, 1966.
- Gedeon, G. S., Tesseral Resonance Effects on Satellite Orbits, Celestial Mech.

 1, #2, 167-189, 1969.

- Gooding, R. H., Lumped Fifteenth-Order Harmonics in the Geopotential, <u>Nature</u>
 Physical Science 231, June 21, 1971a.
- Gooding, R. H., Lumped Geopotential Coefficients $\overline{C}_{15,15}$ and $\overline{S}_{15,15}$ Obtained from Resonant Variation in the Orbit of Ariel 3, Royal Aircraft Establishment Technical Report 71068, Farnborough, Hants., England, 1971b.
- Greene, R. H., A Maneuverable Geodetic Satellite in a Variety of Resonant Orbits, Paper (67-122) Presented at 5th Aerospace Sciences Meeting (AIAA), New York City, January, 1967.
- Jacchia, L. G., Revised Static Models of the Thermosphere and Exosphere with Empirical Temperature Profiles, Smithsonian Astrophys. Obs. Special Report 332, Cambridge, Mass., 1971.
- Jacchia, L. G., Static Diffusion Models of the Upper Atmosphere with Empirical Temperature Profiles, Smithsonian Contributions to Astrophysics Vol. 8, 215-257, 1965.
- King-Hele, D. G., Heavenly Harmony and Earthly Harmonics, Quarterly Journal of the Royal Astron. Soc., 13, 374-395, 1972a.
- King-Hele, D. G., 15th Order Harmonics in the Geopotential from Analysis of Decaying Satellite Orbits, Paper (a.3) Presented to 15th Cospar Meeting, Madrid, Spain, 1972b.
- Lerch, F. J., C. A. Wagner, D. E. Smith, M. L. Sandson, J. E. Brown and J. A. Richardson, Gravitational Field Models for the Earth, Goddard Space

 Flight Center Document X-553-72-146, Greenbelt, Md., 1972a.

- Lerch, F. J., C. A. Wagner, B. H. Putney, M. L. Sandson, J. E. Brownd, J. A. Richardson and W. A. Taylor, Gravitational Field Models Gem 3 and 4, Goddard Space Flight Center Document X-592-72-476, Greenbelt, Md., 1972b.
- Wagner, C. A., The Accuracy of Geopotential Solutions from Resonant Satellite

 Data, Goddard Space Flight Center Document X-553-72-472, Greenbelt, Md.,

 1972a.
- Wagner, C. A., Earth Zonal Harmonics from Rapid Numerical Analysis of Long Satellite Arcs, Goddard Space Flight Center Document X-553-72-341, Greenbelt, Md., 1972b.
- Wagner, C. A., and B. C. Douglas, Resonant Satellite Geodesy by High Speed

 Analysis of Mean Kepler Elements, In: Dynamics of Satellites 1969,

 130-137, Springer Verlag, New York, 1970.
- Wagner, C. A. and B. C. Douglas, Perturbations of Existing Resonant Satellites,
 Planetary and Space Sci. 17, 1505-1517, 1969.

TIME (MJD)	A(e,r.) .	E	INCL (°)	OMEGA (°)	NODE (°)	MEAN(°) }
37315.40140000	1.3328733C	.1889338	33.3590	345.4664	80.0857	8 • 6¢37
37322.0736000	1.33284930	.1891909	33.3539	18.0779	58.1833	347.4229
37329.19580000	1.33284840	. 1894391	33 • 3509	52.8693	34.7932	321+8189
37336.0472CCC0	1.33283000	.1895110	33.3496	86.2779	12.2916	256,0275
37343.C764CCC0	1.33283130	.1894589	33.3514	. 120 .5577	_349+2040	_259.7657
37350.C13900C0	1.33282210	.1891846	33.3549	154.4246	326.4215	217.9871
37357.038900C0	1.33281886	.1889138	33.3576	. 188 • 7666	303.3556	165.4830
37363.07500CC0	1.3328026C	.1887086	33.3580	218.3138	283.5362	127.6701
37370.C125C0C0	1.33279230	.1886048	33.3604	252.2814	260.7574	86.2266
37377.31250000	1.33279500	·1885856	33.3609	288.0567	236.7840	£1.2¢17
37384.C7360CC0	1.3328032C	-1886639	33.3578	321 - 17 30	214.5837	26.3398
37391.01540000	1.3327976C	.1888876	33.3548	355.1591	191.7913	2.0690
37398.137500C0	1.33278350	.1891405	33.3478	29 . 9 7 2 3	168.4014	338.4506
37405.07920000	1.33277590	.1893754	33.3436	63.8645	145.60C0	314.6172
37412.C194C0C0	1.33277130	.1894153	33.3431	97 • 7168	122.7996	285.4247
37419.04720CC0	1.33276740	.1893167	33.3452	132.0024	99.7116	245.4402
	1.33277070	.1890309	33.3525	166 • 31.19	76 - 6347	199.9366
37432.C181C0C0	1.33276780	.1888126	33.3588	195.3802	57.1124	157.6462
37439.94510000	1.33276460	1888506 X-	33.3631	234.0716 X	31.0903	108.8296-X
37447.24440000	1.33275400	.1885528	33.3701%	269.9570	7.1108	69.6480
37452.922200C0	1.33277210	·1885901	33.3620-	297.7801	348.4760	43.5616
37459.7726CCC0	1.33278200	. 1888000 X	33.3606	331.3237	325.9800	20.1626 X
37466.35420CC0	1.33275330	.1890336	33.3568	3.5199	304.37.66	356 • 1937
37473.29580000	1.33274840	.1892910	33.3508	37.4479	281.5719	333.1700
37480.C5690CCO	1.33274500	.1894857	33.3471	70.4289	259.3617	309.8920
37467.C6710CC0	1.3327457C	.1894801	33.3450	104.7219	236.2660	276.1860 X
37494.02360000	1.3327407C	.1893021	33 • 346 1	138.57.58	_ 213.4733	236+8072
37501.C5000C00	1.3327333C	.1890460	33.3517	172.9180	190.3912	192.2477
37508.C7500CC0	1.33273700	.1887792	33.3563	207 .2867	167.3178	142+2167
37515 • 01110000	1.33273860	.1886585	33.3602	241.2648	144.5386	97.4731
37522.04030000	1.33274960	1886274	33.3622	275.6882	121.4591	64 • 0.7.1.8
37529.07080000	1.3327343C	.1887117	33.3609	310.1348	98.3767	36.2700
37536.28190000	1.33273870	.1888820	33.3581	345.4404:	74.6870	9.0038
37543.13C60CC0	1.33272870	.1891593	33.3536	18 .9422	52.1832	346.48E4 🗶
37550.C7500C00	1.33273176	.1893656	33.3501	52.8376	29.3801	324.2267
37557.C15300C0	1.33272910	.1894656	33.3493	86 • 6786	6.5821	296-5466
37564.04310000	1.33271750	. 1893543	33 • 3511	120.9673	343.4563	258-1173
37571.06940000	1.33271720	-1890880	33.3519	155.2623	320.4175	214.184C
37578.CC420000	1.33271280	.1888134	33 .3552	189.1746	. 297.6414	164.4972
37565.03040C00	1.33270560	.1885637	33.3577	223.5681	274.5616	120.7328
37592.C5330CC0	1.332706CC	.1884543	33.3593 -	257 -99 16	251.4825 X-	E2.661.1.X
37599.(8750000	1.33271720	.1884101	33 • 3598	292.4319	228.4019	50.2095
37606.C277C0C0	1.3327205C ==	. 1885289.	33 • 3566	326.427.7	205-6114	23.2350
37613.02360CC0	1.33265570	.1887075	33.3498	1 • 2854 火	182.2281 🗶	356.8670 💢
37620.C00CC000	1.33268370	1890043	33.3464	34 • 7.78 1	159.7237	335.601-1
37627.030560C0	1.33266410	.1891840	33.3412	69.1077	136.6239	309.4771
37634.05970000	1.33267920	.1892017	33.3430	103.3821	113.5257	277. 9536
37641 - 17640000	1.33266380	.1890120	33.3505	138.1212	90.1496	235.7752
						
37648.022200C0	1.33266030	.1887096	33.3566	17.1.5643	67.6649	193.0.739

77662-07220CC0	TIME (MJD)	A(e.r.)	E	INCL (°)	OMEGA (°)	NODE (°)	MEAN (°)
3766,0-28C00C00	37662-07220000	1.33265510	.1882510	33.3621	240 • 3630 ·	21.5250-	57.7260
7766,04033000 1.332649EC .188249I 33.3631 308.8047 335.6641 335.8255. 77690,28190000 1.33261340 .1887299 33.3509 18.5287 288.9013 346.4631 370697.3125000 1.33261310 .1887299 33.3509 18.5287 288.9013 346.4631 370697.3125000 1.33260400 .1891149 33.3420 85.8441 243.5555 256.8415 27711.1000000 1.33260400 .1891149 33.3420 85.8441 243.5555 256.8415 27711.1000000 1.3326060 .1887008 33.3426 120.1283 220.5042 261.6244 377181.37710000 1.3326060 .1887008 33.3436 120.1283 220.5042 261.6244 377181.37710000 1.33250660 .18847008 33.3474 155.7717 1 190.5351 1 161.3244 37733.C7500000 1.33257560 .1884499 33.3557 193.2082 171.3941 161.3244 37733.C7500000 1.33257560 .1882206 33.3553 220.6278 148.2236 115.9753 37740.0111000 1.33257220 .1882206 33.3550 227.6278 148.2236 115.9753 37764.4000000 1.3325320 1.888299 33.3585 297.8335 101.2702							
37690, 28190000							
37690,28190000							
3769-7.312500C0							
37704.07220CC0							
37711.10000000							
37716.377100C0 1.33250540 .1884439 33.3571 193.2082 171.3941 161.3240 X-37733.C7500C00 1.33255540 .1882851 33.3573 193.2082 171.3941 161.3244							
37736,:C5000C00							4
37733.c7500C00						•	·
37740.01113000							
3774.40C00CCO							
37761.06540000							
37761.0C570C00 1.33283A30 1.886698 33.3539 4.4823 56.5590 358.0155 377768.21940C00 1.3328326 1.889563 33.3530 39.7267 32.8746 331.7145 37775.15833000 1.3328326 1.889563 33.3530 39.7267 32.8746 331.7145 37785.26670000 1.332491C0 1.8919A7 33.3480 113.1629 343.4262 266.2726 37790.02220000 1.33247810 1.889744 33.3496 113.1629 343.4262 266.2726 37797.04580C00 1.33247010 1.887133 33.3541 180.4825 298.1464 181.2134 37804.1537C000 1.33245070 1.883967 33.3590 215.3103 × 274.7722 × 128.8071 × 128.807							
37768.21940CCC							
37775.158300C0 1.3325034C .1891580 33.3483 73.5910 10.0757 305.0166 37783.2667C0C0 1.332491C0 .1891437 33.3480 113.1629 343.4262 266.2726 37790.02200C0 1.33247070 .1887133 33.3490 146.1342 321.2277 228.7380 37767.04580CC0 1.3324625C .1884728 33.3500 215.3103 274.7712 128.8071 37811.183300C0 1.33248507C .1883967 33.3599 249.7420 251.6948 87.4780 37818.03060000 1.332448CC .1883967 33.3550 23.2963 229.1963 259.1963 37825.23850CC0 1.3324717C .1886858 33.3550 318.6285 205.5048 27.5673 37832.35830CC0 1.3324471C .1886858 33.3550 353.5044 182.11C8 3.7076 37846.23510000 1.33244730 .1891887 33.3450 61.3546 136.4936 315.3730 37851.62330000 1.3324356C .1892867 33.3554 128.6234 91.1846 250.8955 37867.04310000 1.3324056C .1892867 33.3							
37783.2667,000							
37790.022200C0							
37897.04580CC0 1.33247070 .1887133 33.3541 180.4825 298.1464 181.2134 37804.1537CC00 1.3324625 .1883728 33.3500 215.3103 ★ 274.7752 ★ 128.8071 ★ 37811.183300C0 1.3324507C .1883967 33.3599 249.7420 251.6948 87.4780 37811.813300C0 1.3324485C .1883563 33.3594 283.2963 229.1963 56.7958 37825.23859CC00 1.3324717C .1886858 33.3550 318.6285 205.5048 27.5673 37832.335830CC0 1.3324717C .1886858 33.3506 353.5044 182.11C8 3.7076 37839.5194C000 1.33240100 .1889568 33.3471 28.3407 ★ 158.7110 ★ 340.0747 ★ 37846.23610000 1.3324730 .1891887 33.3450 61.3546 136.4936 315.3730 37853.C8330000 1.3324356C .1892867 33.3455 94.7071 113.9863 255.6604 37860.01940000 1.33242710 .189187 33.3487 128.6234 91.1846 250.8955 3767.04210C00 1.33240540 .1889287 33.3543 162.9326 68.0971 205.5602 37874.065330C0 1.33239261 .188454 33.3605 197.3136 45.0177 154.8537 37881.08890C0 1.33239261 .188454 33.3668 231.7266 21.9365 109.8415 37868.20420000 1.33239261 .1884454 33.3648 231.7266 21.9365 109.8415 37868.20420000 1.33239361 .1883471 33.3642 300.1706 336.0550 41.8641 37902.44030000 1.3324036C .1883868 33.3660 266.6063 358.5553 70.7903 37895.05140CC0 1.3324036C .1883868 33.3662 300.1706 336.0550 41.8641 37902.44030000 1.3324036C .18838069 33.3545 109.3555 288.9680 352.3757 37916.137500C0 1.332393610 .1883871 33.3642 300.1706 336.0550 41.8641 37902.490300 1.33239361 .1883871 33.3642 300.1706 336.0550 41.8641 37902.3793.01040C00 1.332393610 .1888693 33.3565 179.7288 243.6417 301.5326 37973.16530CC0 1.33239360 .1883871 33.3488 43.3983 266.7513 329.1064 3793.106500C0 1.3323786C .1891077 33.3488 43.3983 266.7513 329.1064 3793.7903.37920C00 1.3323785C .1891764 33.3457 77.7288 243.6417 301.5326 37972.16530CC0 1.3323550 .1886530 33.3555 179.7974 174.9562 180.1127 3793.1050000 1.3323785C .1891764 33.3555 179.7974 174.9562 180.1127 3793.1050000 1.3323550C .1881930 33.3555 179.7974 174.9562 180.1127 37955.22080C00 1.3323550C .1881933 33.3560 33.3557 179.7974 174.9562 180.1127 37955.22080C00 1.3323550C .1889363 33.3560 33.3557 124.2089 151.8774 130.9255 37958.015							
37804.1537CC00 1.332462C .1884728 33.3600 215.3103 ★ 274.7752 ★ 128.8071 ★ 37811.183300CC 1.3324507C .1883967 33.3599 249.77420 251.6948 87.4780 37818.03060000 1.332448CC .1883543 33.3594 283.2963 229.1963 56.7958 37825.2385C000 1.332443CC .1883543 33.3594 283.2963 229.1963 56.7958 37825.2385C000 1.33244717C .1886858 33.3550 318.6285 205.5048 27.5673 37832.35830CC0 1.332401C0 .1889568 33.3471 28.3407 ★ 158.7110 ★ 340.0747 ★ 37846.23610000 1.33244730 .1891887 33.3450 61.3546 136.4936 315.3730 37853.08330000 1.33244710 .1891887 33.3450 61.3546 136.4936 315.3730 37853.08330000 1.33242710 .189187 33.3450 94.7671 13.9863 285.6604 37860.01940000 1.3324074 .1891747 33.3487 128.6234 91.1846 250.8955 37867.04210000 1.33240540 .1889273 33.3543 162.9326 68.0971 205.5602 37874.06530CC0 1.3323922 .18868.95 33.3560 197.3136 45.0177. 154.8537 37881.088900C0 1.33239210 .188454 33.3648 231.7266 21.9365 109.8415 37888.20020000 1.3324036 .1883868 33.3660 266.6063 358.5553 70.7903 37899.051400CC0 1.33234036 .1883868 33.3660 266.6063 358.5553 70.7903 37916.137500C0 1.33234036 .1888069 33.3547 10.3585 288.9680 352.3757 37916.137500C0 1.33237840 .1889677 33.3488 43.3983 266.7513 329.1064 37923.16430CC0 1.33237850 .1889643 33.3547 17.7238 243.6417 301.5326 37937.03610000 1.33237850 .1891764 33.3487 77.7238 243.6417 301.5326 3794.05630000 1.33237850 .1891764 33.3467 77.7238 243.6417 301.5326 3794.05630000 1.33237850 .1891764 33.3457 77.7238 243.6417 301.5326 37957.03610000 1.33237850 .1896830 33.3555 179.7974 174.9562 180.1127 3793.0110000 1.33237850 .1896830 33.3551 145.4472 198.0389 229.4203 37950.000000 1.33237850 .1896830 33.3560 248.2026 129.064792.5291 37950.010000 1.33237850 .1896830 33.3560 248.2026 129.064792.5291 37950.010000 1.33237850 .1896830 33.3551 145.4472 198.0389 229.4203 37950.00000 1.33237850 .1898963 33.3560 248.2026 129.064792.5291 37950.010000 1.33237850 .1889630 33.3560 248.2026 129.064792.5291 37950.010000 1.33235510 .18886234 33.3609 351.1043 60.0906 6.3405 379							
37811.183300C0 1.3324507C .1883967 33.3599 249.7420 251.6948 67.4760 37818.03060000 1.332448CC .1883543 33.3594 283.2963 229.1963 56.7958 37825.23850C00 1.33244717C .1886858 33.3550 318.6285 205.5048 27.5673 37832.35830C00 1.3324717C .1886858 33.3506 353.5044 182.11C8 3.7078 37839.5199C000 1.33240710 .1889568 33.3471 28.3407							
37818.03060000 1.332448CC .1883543 33.3594 283.2963 229.1963 56.7958 37825.23850000 1.332443EC .1884626 33.3550 318.6285 205.5048 27.5673 37832.35830000 1.33240100 .18869568 33.3451 28.3407 X 158.7110 X 340.0747 X 37846.23610000 1.33244730 .1891887 33.3450 61.3546 136.4936 315.3730 37853.08330000 1.33242710 .1891887 33.3450 94.7671 113.9863 285.6604 37860.01940000 1.33249710 .1891887 33.3455 94.7671 113.9863 285.6604 37860.01940000 1.33249540 .1892867 33.3457 128.6234 91.1846 250.8955 37874.0653000 1.33249640 .1889273 33.3543 162.9326 68.0971 205.5602 37881.08890000 1.33239610 .1884454 33.3664 231.7266 21.9365 109.8415 37898.05140000 1.33239610 .188368 33.3660 266.6063 388.5553 70.7903 37999.37920000 1.33240350 .1885764					•		
37825.23890000 1.332443 € C .1884626 33.3550 318.6285 205.5048 27.5673 37832.35830000 1.3324717 C .1886858 33.3506 353.5044 182.1108 3.7076 37834.51940000 1.33244730 .1891887 33.3450 61.3546 136.4936 315.3730 37853.68330000 1.3324356 C .1892867 33.3455 94.7671 113.9863 285.6604 37860.01940000 1.3324954 C .1889273 33.3543 162.9326 68.0971 205.5602 37874.06533000 1.3323922 C .1886395 33.3605 197.3136 45.0177 154.86537 37881.08890000 1.3323926 C .1883868 33.3605 197.3136 45.0177 154.86537 37895.05140000 1.3324036 C .1883861 33.3604 231.7266 21.9365 109.88415 37909.37920000 1.3324036 C .1883861 33.3602 200.1706 336.0550 41.8661 37930.10140000 1.3323740 C .1889069 33.3547 10.3585 288.9680 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
37832.35830CC0							
37839.5194C0C0							
37846.23610000 1.3324350 1.891887 33.3450 61.3546 136.4936 315.3730 37853.08330000 1.3324356 1.892867 33.3455 94.7671 113.9863 285.6604 37867.04310000 1.33242710 1.891747 33.3487 128.6234 91.1846 250.8955 37867.04310000 1.33240540 1.889273 33.3553 162.9326 68.0971 205.5602 37874.06633000 1.33239610 1.88454 33.3605 197.3136 45.0177 164.8537 37881.08890000 1.33239610 1.88454 33.3668 231.7266 21.9365 109.8415 37868.20420000 1.3323966 1.88454 33.3668 231.7266 21.9365 109.8415 37868.20420000 1.3323966 1.883871 33.3642 300.1706 336.0550 41.8641 37902.44030000 1.33240360 1.88586 33.3660 266.6063 358.5553 70.7903 37909.37920000 1.33240360 1.88564 33.3610 336.3826 311.7719 15.1551 37909.37920000 1.33240360 1.888069 33.3547 10.3585 288.9680 352.3757 37916.13750000 1.33237440 1.890677 33.3488 43.3983 266.7513 329.1064 37923.16630000 1.33237850 1.891764 33.3461 111.5700 220.8372 268.1942 37930.10140000 1.33237850 1.891764 33.3461 111.5700 220.8372 268.1942 37930.10140000 1.33237850 1.891764 33.3461 111.5700 220.8372 268.1942 37934.05630000 1.33237850 1.891764 33.3461 111.5700 220.8372 268.1942 37951.08060000 1.33237850 1.886530 33.3551 11.40430 1.4000 1.33237850 1.886530 33.3551 214.2089 151.8774 130.9255 37958.01830000 1.33235400 1.882890 33.3561 248.2026 129.0647 32.62591 37958.01830000 1.33235400 1.882890 33.35610 248.2026 129.0647 32.62591 37958.01830000 1.33235400 1.883963 33.3561 248.2026 129.0647 32.62591 37958.01830000 1.33235400 1.883963 33.35619 283.5529 105.4001 55.2962 37972.15830000 1.33235400 1.883963 33.35619 283.55429 105.4001 55.2962 37972.15830000 1.33235500 1.886234 33.35619 283.55429 105.4001 55.2962 37972.15830000 1.33235150 1.886234 33.35619 283.55429 105.4001 55.2962 37972.15830000 1.33235150 1.886234 33.35619 283.55429 105.4001 55.2962 37972.15830000 1.33235500 1.886234 33.35619 283.55429 105.4001 55.2962 37972.15830000 1.33235500 1.886234 33.35619 283.55429 105.4001 55.2962 37972.15830000 1.33233500 1.886628 33.35619 33.3551 61.5918 12.7056 215.0049					_		
37853.08330000 1.3324356C .1892867 33.3455 94.7671 113.9863 285.6604 37860.01940000 1.3324271C .1891747 33.3487 128.6234 91.1846 250.8955 37867.04310000 1.3324054C .1889273 33.3543 162.9326 68.0971 25.5602 37874.0653000 1.3323922C .1886395 33.3605 197.3136 45.0177 154.8537 37881.08890000 1.3323926C .1883868 33.3660 266.6063 358.5553 70.7903 37895.0540000 1.3324036C .1883871 33.3642 300.1706 336.5553 70.7903 37999.37920000 1.3324036C .1883674 33.3610 336.3826 311.7719 15.1551 37999.37920000 1.3323744C .1890677 33.3488 43.3983 266.7513 329.1064 37923.16530000 1.33233785C .1891674 33.3487 77.7238 243.6417 301.5326 37937.03610000 1.33233785C .1891764 33.3457 77.7238 243.6417 301.5326 37937.03610000 1.33233785C .189164 33.355							
37860.01940000 1.3324271C .1891747 33.3487 128.6234 91.1846 250.8955 37867.0431000 1.3324046 .1889273 33.3543 162.9326 68.0971 205.5602 37874.0653000 1.3323921C .1886395 33.3605 197.3136 45.0177 154.8537 37881.0889000 1.33239610 .1884454 33.3608 231.7266 21.9365 109.8415 37868.20420000 1.33239610 .1884854 33.3660 266.6063 358.5553 70.7903 37895.05140000 1.33240330 .1883871 33.3642 300.1706 336.0550 41.8641 37902.4403000 1.33240330 .1885764 33.3642 300.1706 336.0550 41.8641 37909.3792000 1.33240330 .1885764 33.3610 336.3826 311.7719 15.1551 37909.3792000 1.33240330 .188569 33.3547 10.3585 288.9680 252.3757 37916.13750000 1.33237440 .1890677 33.3488 43.3983 266.7513 329.1064 37923.16530000 1.33237850 .1890677 33.3488 43.3983 266.7513 329.1064 37937.03610000 1.33237850 .1891764 33.3461 111.5700 220.8372 288.1942 37937.03610000 1.33237140 .1889643 33.35516 145.4472 198.0385 229.4203 37944.05630000 1.33237140 .1889643 33.35516 145.4472 198.0385 229.4203 37944.05630000 1.3323510 .1884309 33.35516 145.4472 198.0385 229.4203 37951.08060000 1.3323510 .1884309 33.3551 145.4472 198.0385 229.4203 37955.22080000 1.3323540 .1884309 33.3551 145.4472 198.0385 229.4203 37955.22080000 1.3323510 .1884309 33.3501 288.2026 129.0647 92.5291							
37867.04310000 1.3324094C .1889273 33.3543 162.9326 68.0971 205.5602 37874.06533000 1.3323922C .1886395 33.3605 197.3136 45.0177 154.8537 37881.08890000 1.3323926C .1884454 33.3608 231.7266 21.9365 109.8415 37885.05140000 1.3323926C .1883868 33.3660 266.6063 358.5553 70.7903 37895.05140000 1.33240030 .1883871 33.3642 300.1706 336.0550 41.8641 37902.4403000 1.33240360 .1885764 33.3610 336.3826 311.7719 15.1551 37916.1375000 1.33237440 .1880699 33.3547 10.3585 288.9680 352.3757 37923.16530000 1.33237840 .1891764 33.3488 43.3983 266.7513 329.1064 37930.10140000 1.33237140 .1891764 33.3481 111.5700 220.8372 268.1942 37944.05630000 1.33235110 .1886530 33.3556 179.7974 174.9562 180.1127 37951.08060000 1.33235402 .1884309 33.35							
37874.06€30CC0 1.3323922C .1886395 33.3605 197.3136 45.0177 154.8537 37881.088900C0 1.33239610 .1884454 33.3648 231.7266 21.9365 109.8415 37888.20420000 1.3323926C .1883688 33.3660 266.6063 358.5553 70.7903 37895.05140CC0 1.3324033C .1883671 33.3642 300.1706 336.0550 41.8641 37902.44030000 1.3324035C .1885764 33.3610 336.3826 311.7719 15.1551 37909.37920000 1.3323744C .1880677 33.3488 43.3983 266.7513 329.1064 37930.10140C00 1.3323745C .1890677 33.3488 43.3983 266.7513 329.1064 37930.10140C00 1.3323785C .1891764 33.3461 111.5700 220.8372 248.1942 37944.05€30000 1.3323765C .1889643 33.3516 145.4472 198.0385 229.4203 37951.0860000 1.3323501C .1886530 33.3555 179.7974 174.9562 180.1127 37958.01530000 1.33235420 .1884309 33.							
37881.088900C0 1.33239610 .1884454 33.3648 231.7266 21.9365 109.8415 37888.20420000 1.3323926C .1883868 33.3660 266.6063 358.5553 70.7903 37895.05140CC0 1.3324003C .1883871 33.3642 300.1706 336.0550 41.8641 37909.37920C00 1.3324035C .1885764 33.3610 336.3826 311.7719 15.1551 37909.37920C00 1.3323744C .1890677 33.3488 43.3983 266.7513 329.1064 37923.16530CC0 1.3323785C .1891764 33.3461 111.5700 220.8372 288.1942 37937.03610C00 1.3323785C .1891764 33.3516 145.4472 198.0385 229.4203 37937.03610C00 1.3323785C .1889643 33.35516 145.4472 198.0385 229.4203 37944.05830000 1.33233501C .1884509 33.3551 147.9774 174.9662 180.1127 37955.02080000 1.3323540 .1884309 33.3501 248.2026 129.0647 .92.5291 37972.15830000 1.3323540 .1883							
37888.20420000 1.3323926C .1883868 33.3660 266.6063 358.5553 70.7903							
37895.05140CC0							
37902.44030000 1.33240350 .1885764 33.3610 336.3826 311.7719 15.1551 37909.37920000 1.33240360 .1888069 33.3547 10.3585 288.9680 352.3757 37916.13750000 1.33237440 .1890677 33.3488 43.3983 266.7513 329.1064 37923.16530000 1.33238340 .1892121 33.3457 77.7238 243.6417 301.5326 37930.10140000 1.33237850 .1891764 33.3461 111.5700 220.8372 268.1942 37937.03610000 1.33237140 .1889643 33.3516 145.4472 198.0385 229.4203 37944.05830000 1.33236530 .1886530 33.35555 179.7974 174.9562 180.1127 37951.08660000 1.33235010 .1884309 33.3591 214.2089 151.8774 130.9255 37958.01530000 1.33235460 .1883134 33.3619 283.5429 105.4001 55.2962 37972.15830000 1.33235150 .1886234 33.3609 317.5468 82.6005 28.1765 37996.3250000 1.33233190 .1886234							
37909.37920000 1.3324036C .1888069 33.3547 10.3585 288.9680 352.3757 37916.13750000 1.3323744C .1890677 33.3488 43.3983 266.7513 329.1064 37923.16530000 1.3323785C .1891764 33.3461 111.5700 220.8372 248.1942 37937.03610000 1.3323714C .1889643 33.3516 145.4472 198.0385 229.4203 37944.05630000 1.33233653 .1886530 33.35555 179.7974 174.9662 180.1127 37951.08660000 1.33235010 .1884309 33.3591 214.2089 151.8774 130.9255 37965.22080000 1.33235420 .1882890 33.3610 248.2026 129.0647							
37916.137500C0 1.3323744C .1890677 33.3488 43.3983 266.7513 329.1064							
37923.16530CC0 1.33238340 .1892121 33.3457 77.7238 243.6417 301.5326 37930.10140C00 1.3323785C .1891764 33.3461 111.5700 220.8372 268.1942							
37930.10140C00 1.3323785C .1891764 33.3461 111.5700 220.8372 268.1942—— 37937.03610000 1.3323714C .1889643 33.3516 145.4472 198.0386 229.4203 37944.05630000 1.3323653C .1886530 33.3555 179.7974 174.9562 180.1127 37951.08060000 1.3323501C .1884309 33.3591 214.2089 151.8774 130.9255 37958.01530000 1.3323542C .1882890 33.3610 248.2026 129.0647							
37937.03610000 1.3323714C .1889643 33.3516 145.4472 198.0385 229.4203 37944.05630000 1.3323663C .1886530 33.3555 179.7974 174.9662 180.1127 37951.08060000 1.3323501C .1884309 33.3591 214.2089 151.8774 130.9255 37958.01630000 1.3323452C .1882890 33.3610 248.2026 129.0647							
37944.05£30000 1.3323653C .1886530 33.3555 179.7974 174.9562 180.1127 37951.08060CC0 1.3323501C .1884309 33.3591 214.2089 151.8774 130.9255 37958.01£30CC0 1.3323452C .1882890 33.3610 248.2026 129.0647							
37951.08060CC0 1.3323501C .1884309 33.3591 214.2089 151.8774 130.9255 37958.01530CC0 1.3323452C .1882890 33.3610 248.2026 129.0647 92.5291							
37958.01530CC0 1.3323452C .1882890 33.3610 248.2026 129.0647							
37965.22080000 1.33235460 .1883134 33.3619 283.5429 105.4001 55.2962 37972.15830000 1.33235220 .1883963 33.3629 317.5468 82.6005 28.1765 37979.00000 1.33235150 .1886234 33.3609 351.1043 60.0906 6.3405 37986.30560000 1.33233190 .1888628 33.3571 26.8248 36.1025 340.9922 37993.42360000 1.33235680 .1891355 33.3531 61.5918 12.7056 215.0499							
37972.15830CC0 1.33235220 .1883963 33.3629 317.5468 82.6005 28.1765 37979.CC690000 1.3323515C .1886234 33.3609 351.1043 60.0906 6.3405 37986.3C560000 1.33233190 .1888628 33.3571 26.8248 36.1025 340.9922 37993.4236CCC0 1.3323568C .1891355 33.3531 61.5918 12.7056 215.0499							
37979.CC690000 1.3323515C .1886234 33.3609 351.1043 60.0906 6.3405 37986.3C560000 1.33233190 .1888628 33.3571 26.8248 36.1025 340.9922 37993.4236CCC0 1.3323568C .1891355 33.3531 61.5918 12.7056 215.0499							
37986.30560000 1.33233190 .1888628 33.3571 26.8248 36.1025 340.9922 37993.42360000 1.33235680 .1891355 33.3531 61.5918 12.7056 215.0499							
37993.42360000 1.33235680 .1891355 33.3531 61.5918 12.7056 215.0499							

33.3538

1 28 •00 50

327.5857

249.6060

0

38007.02500000

1.33232920

•1891082

TIME (MJD)	A(e.r.)	E	INCL (°)	OMEGA (°)	- NODE (°)	MEAN (°)
380.14.04E60CCO	1.33232990	1888638	33.3577	162.34.70	304.8959	206.8161
38021.07080000	1.33233530	.1885873	33.3611	196 • 7137	281.6159	158.5302
8028.00280000	1.33234000	· 1884301	33.3623	230.6808	259.0340	_109.7733
38035.02770CC0	1.33233980	.1883346	33.3621	265.1217	235.9442	72.4411
18042.2347CC00	. 1.33233590-	-1884105	33.3602	300 • 453 · 1	212.2558	41.4151
8049.35280CCO	1.3323266.0	.1885506	33.3588	335.3496	188.6573	15.5946
8056.02080CCO-	1.33232410	1888018	33.3548	8 .00.7-1	166.9372	_353.5254
8063.31940000	1.33232590	.1890766	33.3504	43.7070	142.9408	328.6016
8070-16670000-	1.33232850	.1892594	33.3496	77 • 1366	_120.4296	301.831.9
8C77.012500C0	1.33232330	.1892573	33.3512	1 10 • 560 8	97.9171	269.5379
8084.03610000	1.33232400	1890645	33.3539	144.8659	7.4.8247	226.9325
8001.05830000	1.33232630	.1887843	33.3596	179.2117	51.7367	178.7472
8098 • 1.7(80000	1.3323401.0		33.3644	214.0384	28.3594	130.7928
8105.01530000	1.33233590	.1884451	33.3672	247.5866	5.8642	92.7024
8112.13060000			33.3675		342.4831	55.7253
8119.06810000	1.33233360	.1885267	33.3626	316.4805	319.6889 X	29.0994
8126.45690CCO	1.33233310	.1887152	33 • 3597	352.6793	295.3962	4.391-1
8133.034700C0	1.33231310	.1889617	33 • 3527	24.8672	273.7702	341.8879
814015280CCO	1.33233820		33.3489	59 • 6378	250.3647	316.1156
8147.05C200C0	1.33233460	.1892242	33.3479	93.4926	227.5519	289.6278
	1.33233460	.1890778	33.3502		204.7532	252.0584
8154.02500.000		.1887773	33.3511	161.6865	181.6701	203.7764
8161.04720000	1.33232650		33•3533	196 • 0 6 6 9	158.5857	155.4157
8168.C6\$40CCO	1.33233210	1885076				
8175.00280000	1.33232960	.1882938	33.3564	230.0448	135.7940	112.1818
8182.027700C0	1.332328\$0	.1882247	33.3602	264.4876	112.7054	74+8950
8189.01250000	1.33234090	.1882292	33.3632	298 • 9408 🗶	89.6147	43.1514 💢
8196.08190000		1883934	33.3613	333.3817	66.5227	17.0800
8203.02080000	1.332354CC	.1886008	33.3572	7.3651	43.7194	356.1778
8210.0486000	1.33230060	.1888099	33.3513		20.6216	330 • 136E
8217.07640000	1.33231920	.1889815	33.3483	76.0430	357.5176	304.1323
8224.01250000	1.3323216C	.1889152	33.3486		334.7184	272+2903
8231.03€10000	1.33232740	.1887136	33.3515	144 • 2092	311.6322	229.7370
8238.05830000	1.33232240	. 1884113		178 • 5567		181.5936
8245 - 1 7080000	1.33232250	.1882012	33.3540	213.3961	265.1796	133.7755
8252.01390000	1.33231940	.1880606				90.447.7
8259.04030000	1.33231340	.1880377	33.3547	281.3978	219.5952	59.0449
8266.33750000	1.33230800	1880918	33 • 35 53	· ·	195.6168	28.8721
8273.00560000	1.33232220	.1882878	33.3525	349.8621	173.7000	7.2560
8280.12360000	1.332328CC	• I 885691 ·-	33.3469	24.7084	- 150.3082	342.0830
8287.24170000	1.33229760	.1888168	33.3432	59 • 49 17	126.9083	317.0539
8294.26810000	1.332302CC	.1889007	33.3426	93.8050	103.8057	266.3385
8301.08940000	1.33226750	.1887826	33.3444	127 • 2211 X	81.3057 X	249.6067 X
8308.04580CCO	1.33228840	·1885688 ·	33.3500 -	161.1190	58+5117 = -	207-7894
8315.06670000	1.33228300	•1882687	33,3566	195 4839	35.4364	155.3100
8322.09030000	1.33226540	.1881288	33.3613	. 229.9108	12.3563	114.2025
8329.02360000	1.33225570	.1880518	33.3619	263.9132	349.5767	73.0303
8336.05000000	1.3322506C	.1881229	33.3586	298 • 3649	326-4754	- 43.6458
8343.42590000	1.33222770	.1882691	33.3544	334.5970 X	302.1943 X	16.1249)
8350.01530000	1.33223630	.1885452	33.3504	6.8094	280 - 5666	356.2871.
38357.4028CCC0	1.33221860	.1888677	33.3430	42.9380	256.2807	329.3339

TIME (MJD)	A(e.r.)	E	INCL (°)	OMEGA (°)	NODE (°)	MEAN (°)
38364.06540000	1.33224250	.1890459	33.3416	75.4874	234 . 3596	364.9032
38371.0041CCC0	1.33222850	.1890407	.33 • 3396	109.3499	211.5515	270.8312
38378.16670000	1.33220950	.1888115	33.3402	143.6613 X	188.4539 X	231 • 7401-X—
38365.04660000	1.33220860	.1885578	33.3457	178 •0 137	165.3642	181.5490
38392.15970000	1.33221040	·1882899 ·	33.3519	212.8680	141.9805	131.8222
38399.00280000	1.33220620	.1881985	33.3564	246.4287	119.4854	92.0516
384C6.747200C0	1.33217870	.1881853	33.3577	284.4192	94.0267-	51 - 1773
38413.05420000	1.33219360	.1883145	33.3567	315.3439	73.2925	31.3351
38430.08190000	1.33216770	.1889216	33.3470	38.7237	17.2992	334.4366
38434.04580000	1.33216560	.1890397	33.3457	58.0989	4.2640	320.3200
38441.07080000	1.33219010	.1890891	33.3446	92.3946	341.1614	287.8939
38448.18410CCO	1.33217060	.1889897	33.3445	127.1437	317.7642	250.4623 🗶
38469.06940000	1.33216490	.1882337	33.3509	229.4007	249.0827	113.6304
38476.00280000	1.33216110	.1881533	33.3518	263.4100	226.2846	75.6520
38483.0278CCC0	1.33217190	.1881714	33.3535	297.8811	203.1864	43 • 560 8
38490.14440000	1.33216440	.1883088	33.3491	332.7771	179.7879	17.5845
38497.08190000	1.33216540	·1885342	33.3445	6.7804	156.9748	356.3511
38504.19860CCO	1.33216020	.1887957	33.3393	41.6026	133.5663	330.5612
38511.44440000	1.33214960	·1889608	33.3365	75.0650 X	111.0468 X	303.5337. X
38518.06940000	1.33215430	.1889299	33.3392	109.3747	87.9359	271.9805
38525.09170000	1.33215910	•1887574	33.3435	143.6897	64.8452	229.3736
38532.11250000	1.33215820	•1881720 X	33.3483	178 •0657 X	41.7576	181.1557
38539.04310000	1.33215610	·1873837 🗶	33.3668 X	212.1216 🗶	18.9379 🗶	132.4016
38546.1556CCC0	1.33214370	.1880374	33.3557	246.8997	355.5901	90.0890
38553.000C0CC0	1.33215520	.1880127	33.3554	280.4723	333.0904	57.6C32
38560.55830000	1.33215410	.1881506	33.3521	322.4778 🗶	304.9457 🗶	28•1247 🗶
38567.41390000	1.33214076	.1883386	33.3475	351.1806	285.6970	7.4338
38574.35000CC0	1.33214850	.1886468	33.3407	25 • 149 4	262.8907	341.0547
38581.01670000	1.33214330	.1888640	33.3367	57.7366	240.9631	218.9138.
38588.13190000	1.3321433C	·1889669	33.3319	92.5004	217.5553	287.9681
38595.06530000	1.33214390	.1888354	33.3340	1 26 • 3759	194.7475	250.5997
38602.08750000	1.33215130	•1885981	33.3390	160.7191	171.6499	208.0981
STANDARD OBSERVATION	N				•	
SIGMAS	C.00C010CC	0.0000200	0.000500	0.02000	0.020000	1.000000

^{*}These elements were originally determined (by T. Heuring) as osculating values from a precision tracking program (GEODYN) using the precisely reduced Baker-Nunn optical observations of the Smithsonian Astrophysical Observatory's World Wide Network. The mean elements are these osculating values less the short period terms (due to oblateness) due to D. Brouwer, 1959. The aic lengths to which these original elements apply are generally 7 days. After processing the 3-1/2 year arc of mean elements it was found necessary to discard only 48 or 4.4% of these observations. The rejected values are marked with an X.

Table 2
Results of ROAD-Vanguard 3 Orbit Determinations
(Using 3-1/2 Years of GSFC Mean Elements*)

Field	Overall	Weighted Element Residuals (rms)						
Used	Weighted RMS Residual	e (2 × 10 ⁻⁵)	I (0,0005°)	ω (0.02°)	Ω (0.02°)	M (1.°)	Unit Wts.	
SAO SE2 Without Resonant Terms	3.17	2.29	6.79	0.75	1.16	0.7		
SAO SE2 With Resonant Terms	2 . 19	1.44	4.49	1. 06	0.89	0.8		
GEM 4 With Resonant Terms	2.78	1.83	5.92	1.07	1.03	0.8		
SAO SE2 With Resonant Terms + (15, 11) Adjusted From data	1.13	0.76	1.59	1.13	0.73	0.7		
SAO SE2 With Res. Terms + (17, 11) Solved from Constraint	1.14	0.73	1.59	1.19	0.75	0.7		

^{*}All orbit determinations used all six mean elements as observed data and adjusted the six initial elements, a radiation pressure and drag coefficient and 5 mean anomaly "Secular" terms. Included are short and long period luni-solar terms to the 4th degree in their disturbing potentials, as well as all significant long period zonal variations in the given fields and the effects of precession and nutation of the earth's polar axis.

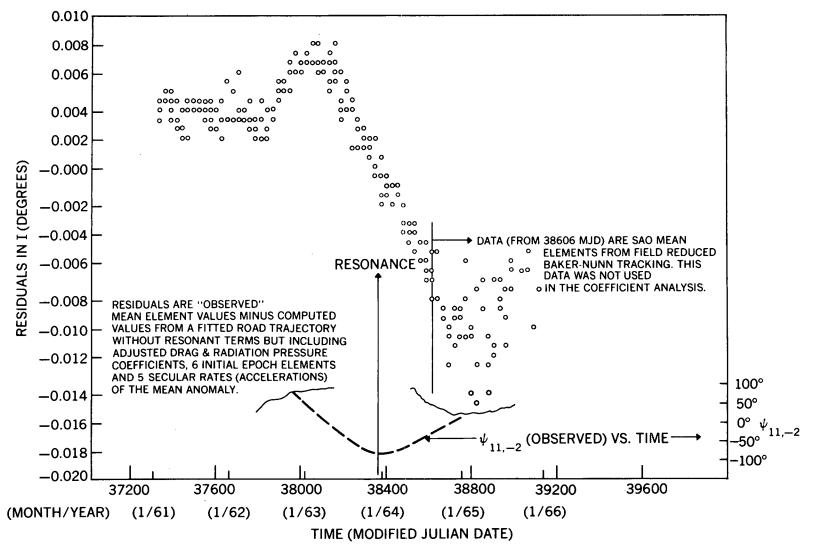


Figure 1. Measurement Residuals In Inclination From A Five Year Nonresonant Vanguard 3 Trajectory

Figure 2. Inclination Residuals From Two 5 Year Simulated Vanguard 3 Trajectories

0.00020

37200

37600

Figure 3. Measurement Residuals In Eccentricity From a 5 Year Nonresonant Vanguard 3 Trajectory*

38400

TIME (MODIFIED JULIAN DATE)

38800

39200

39600

38000



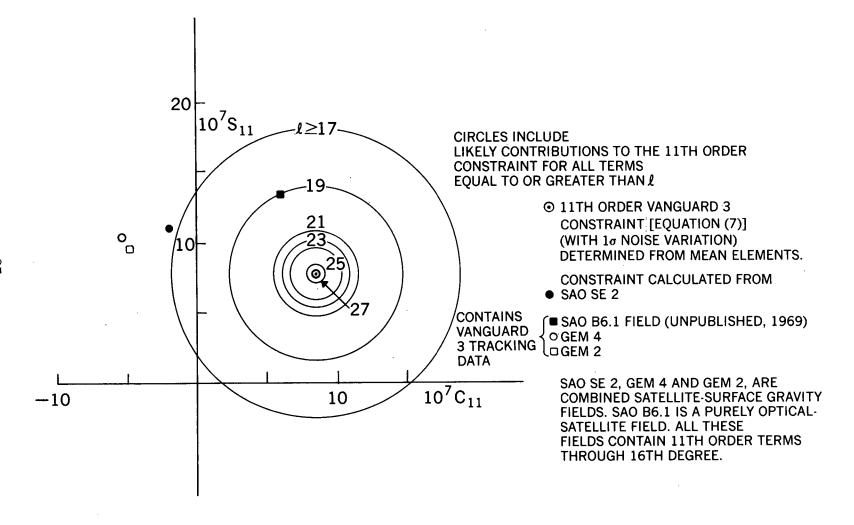


Figure 4. Vanguard 3 Constraint From Various Fields